Compressed Liquid and Supercritical Densities of 1,1,1,2,3,3,3-Heptafluoropropane (R227ea)

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Densities of 1,1,1,2,3,3,3-heptafluoropropane (R227ea) have been measured with a computer-controlled high-temperature high-pressure vibrating-tube densimeter system (DMA-HDT) in the sub- and supercritical states. The densities were measured at temperatures from 278 to 473 K and pressures up to 30 MPa (overall 257 data points), whereby a density range between 285 and 1588 kg \cdot m⁻³ was covered. The uncertainty in the density measurement was estimated to be better than ± 0.2 kg \cdot m⁻³. The experimental data of R227ea were correlated with a virial-type equation of state (EoS) and compared with published data. A comparison is also made with a recent wide-range dedicated equation of state for R227ea.

KEY WORDS: density; equation of state; R227ea; vibrating tube densimeter.

1. INTRODUCTION

A reliable knowledge of the $P\rho T$ behavior of pure compounds and mixtures is of great interest in many fields of research as well as in industrial practice. The densities of fluids as a function of temperature, pressure, and composition are particularly important for the design of industrial plants, pipelines, and pumps. Furthermore, accurate experimental density data are the basis for the development of new correlation equations and improved equations of state (EoS). Information about the $P\rho T$ behavior and ideal gas heat capacities allow the calculation of phase equilibria and other

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thermodynamic properties such as enthalpies, entropies, heat capacities, and heats of vaporization at given conditions (temperature, pressure, and composition). These data are needed for solving material and energy balance equations required for the design and optimization of chemical processes.

Since the beginning of 2001 the use of any chlorofluorocarbons (CFCs) has been prohibited in Europe because of their threat to the ozone layer [1]. Also, the use of some hydrochlorofluorocarbons (HCFCs) was forbidden and the ban will be extended to further HCFCs in the near future. An alternative group of refrigerants includes the hydrofluorocarbons (HFCs) such as 1,1,1,2,3,3,3-heptafluoropropane (R227ea). They have been developed as a group of zero ozone-depletion refrigerants. The greenhouse gas potential of HFCs is in most cases much lower than that for HCFCs and CFCs. Since the beginning of the 1990s, R227ea has been produced in large scale and used as a propellant for medical aerosols, particularly for asthma sprays, and for fire extinguishers.

For R227ea only a few experimental density data in the vapor, compressed liquid, and supercritical states are available in the literature [2–6]. Due to the limited temperature and pressure range covered by these data, experimental investigations were performed here by means of a vibrating tube densimeter. The data are presented in comparison to correlated values using a virial-type EoS and to the experimental data of other authors.

2. EXPERIMENTAL

1,1,1,2,3,3,3-heptafluoropropane (R227ea, Solkane 227 pharma from Solvay, C_3HF_7 , M = 170.03 g/mol, CAS-RN 431-89-0) was supplied without inert components (e.g., air) and used without further purification. The purity (> 99.9 mass%) was checked by gas chromatography.

A computer-operated vibrating tube densimeter system for high temperatures and pressures (temperatures from 273 to 623 K and pressures up to 40 MPa) was used for the measurement of the density data for R227ea. The automated equipment can be used for the determination of densities in the sub- and supercritical states. With this apparatus, a large number of data points can be obtained in a rather short time with a minimum amount of manual effort. A temperature and pressure program can be used to obtain a complete $P\rho T$ field for the desired component. The data of several liquids and liquefied gases (toluene, carbon dioxide, carbonyl sulfide, hydrogen sulfide, sulfur hexafluoride, and dinitrogen monoxide) have already been published [7, 8]. Comparisons with reference EoS for toluene, CO_2 , and SF_6 demonstrated the high accuracy and suitability of this measurement system.

The apparatus and procedure of the measurements were described in detail by Ihmels and Gmehling [7]. A prototype of a high-pressure hightemperature vibrating tube densimeter (DMA-HDT) is the essential part of the experimental setup. The temperature is measured using a Pt100 resistance thermometer and the pressure is monitored by means of a calibrated external pressure sensor (Model PDCR 911, pressure range 60 MPa, Druck). The density values are obtained from the periods of oscillation of the vibrating tube. For the calibration the period of oscillation at zero pressure and for the two reference substances water and butane was used in the investigated temperature and pressure range. The reference densities were calculated using the reference EoS from Pruß and Wagner [9, 10] for water and the EoS from Younglove and Ely [11] for butane. The measured data are subject to experimental errors. The uncertainty of the temperature measurement is estimated to be +0.03 K, and the measurement of pressure has an estimated uncertainty of ± 6 kPa. A maximum error of ± 0.2 kg \cdot m⁻³ exists for density measurements in the temperature and pressure range covered (278 to 473 K, 1 to 40 MPa). For the measured densities between 300 and 1500 kg \cdot m⁻³ this leads to relative errors between $\pm 0.07\%$ and $\pm 0.015\%$. The estimated errors are based on the comparison of experimental data for reference substances (other than those used for calibration) and established literature data [7, 8]. Because of the strong pressure dependence of the densities near the critical point, higher deviations are obtained in this region. With an uncertainty in pressure of ± 6 kPa, a maximum error in density of about $\pm 0.5\%$ in the supercritical region $(T > T_c)$ near the critical pressure and of about $\pm 2\%$ in the region near the critical point is estimated.

3. RESULTS AND DISCUSSION

In this work, the densities of R227ea were measured from 278 to 473 K and from 0.9 up to 30 MPa. The results (257 data points) are listed in Table I and presented graphically in Fig. 1. In the compressed liquid state, densities of R227ea have already been measured from 205 K to the critical temperature, and up to pressures of 51 MPa [2, 3, 5]. In the supercritical region, data are available up to 423 K and 50 MPa [4, 5]. With the new measurements the temperature range was extended up to 473 K. $P\rho T$ data have also been published for the vapor phase [5, 6]. The range of all available density data from the different references are represented in Figs. 2 and 3.

 Table I. Experimental Densities of 1,1,1,2,3,3,3-Heptafluoropropane (R227ea)

| <i>T</i> (K) | P (MPa) | $ ho$ (kg \cdot m ⁻³) | <i>T</i> (K) | P (MPa) | $ ho (\mathrm{kg} \cdot \mathrm{m}^{-3})$ |
|--------------|---------|-------------------------------------|--------------|---------|---|
| 278.24 | 0.916 | 1470.85 | 308.25 | 4.979 | 1382.27 |
| 278.24 | 4.982 | 1492.63 | 308.25 | 9.982 | 1416.79 |
| 278.24 | 9.984 | 1516.00 | 308.25 | 14.984 | 1445.23 |
| 278.24 | 14.985 | 1536.61 | 308.25 | 19.983 | 1469.69 |
| 278.24 | 19.988 | 1555.17 | 308.25 | 24.986 | 1491.33 |
| 278.24 | 24.990 | 1572.14 | 308.25 | 29.987 | 1510.83 |
| 278.24 | 29.985 | 1587.77 | 313.15 | 1.433 | 1329.64 |
| 283.24 | 1.003 | 1452.30 | 313.15 | 4.979 | 1362.70 |
| 283.24 | 4.984 | 1475.19 | 313.15 | 9.981 | 1399.75 |
| 283.24 | 9.984 | 1500.02 | 313.15 | 14.984 | 1429.81 |
| 283.24 | 14.985 | 1521.70 | 313.15 | 19.983 | 1455.44 |
| 283.24 | 19.987 | 1541.12 | 313.15 | 24.987 | 1477.98 |
| 283.24 | 24.987 | 1558.76 | 313.15 | 29.996 | 1498.18 |
| 283.24 | 29.990 | 1574.99 | 318.15 | 5.022 | 1342.85 |
| 288.24 | 1.055 | 1433.09 | 318.15 | 9.985 | 1382.09 |
| 288.24 | 4.983 | 1457.44 | 318.15 | 14.989 | 1413.96 |
| 288.24 | 9.983 | 1483.84 | 318.15 | 19.982 | 1440.82 |
| 288.24 | 14.983 | 1506.68 | 318.15 | 24.988 | 1464.33 |
| 288.24 | 19.985 | 1526.99 | 318.15 | 29.988 | 1485.30 |
| 288.24 | 24.992 | 1545.36 | 323.15 | 5.020 | 1320.64 |
| 288.24 | 29.987 | 1562.19 | 323.15 | 9.978 | 1364.02 |
| 293.25 | 1.114 | 1413.40 | 323.15 | 14.994 | 1397.91 |
| 293.25 | 4.979 | 1439.29 | 323.15 | 20.008 | 1426.23 |
| 293.25 | 9.984 | 1467.44 | 323.15 | 24.989 | 1450.61 |
| 293.24 | 14.985 | 1491.54 | 323.15 | 29.994 | 1472.40 |
| 293.25 | 19.985 | 1512.80 | 328.15 | 5.022 | 1298.86 |
| 293.24 | 24.986 | 1531.93 | 328.15 | 9.980 | 1345.69 |
| 293.25 | 29.992 | 1549.38 | 328.15 | 14.980 | 1381.58 |
| 298.25 | 1.180 | 1393.16 | 328.15 | 19.983 | 1411.28 |
| 298.25 | 4.985 | 1420.77 | 328.15 | 24.991 | 1436.86 |
| 298.25 | 9.986 | 1450.82 | 328.15 | 29.979 | 1459.38 |
| 298.25 | 14.983 | 1476.25 | 333.15 | 1.914 | 1230.58 |
| 298.25 | 19.986 | 1498.52 | 333.15 | 4.978 | 1275.61 |
| 298.25 | 24.987 | 1518.44 | 333.15 | 9.980 | 1327.14 |
| 298.25 | 29.989 | 1536.56 | 333.15 | 14.986 | 1365.25 |
| 303.25 | 1.255 | 1372.36 | 333.15 | 19.986 | 1396.42 |
| 303.25 | 4.978 | 1401.74 | 333.15 | 24.983 | 1423.06 |
| 303.25 | 9.984 | 1433.95 | 333.15 | 29.987 | 1446.50 |
| 303.25 | 14.985 | 1460.82 | 338.14 | 2.061 | 1202.92 |
| 303.25 | 19.987 | 1484.16 | 338.14 | 4.980 | 1251.69 |
| 303.25 | 24.987 | 1504.92 | 338.14 | 9.980 | 1307.95 |
| 303.25 | 30.019 | 1523.83 | 338.14 | 14.986 | 1348.59 |
| 308.25 | 1.296 | 1350.55 | 338.14 | 19.986 | 1381.41 |

| <i>T</i> (K) | P (MPa) | $ ho (\mathrm{kg} \cdot \mathrm{m}^{-3})$ | <i>T</i> (K) | P (MPa) | $ ho (\mathrm{kg} \cdot \mathrm{m}^{-3})$ |
|--------------|---------|---|--------------|---------|---|
| 338.14 | 24.984 | 1409.22 | 368.13 | 29.993 | 1355.36 |
| 338.14 | 29.989 | 1433.54 | 373.12 | 3.521 | 949.52 |
| 343.14 | 2.229 | 1173.81 | 373.13 | 4.978 | 1037.05 |
| 343.14 | 4.982 | 1226.65 | 373.13 | 9.985 | 1160.32 |
| 343.14 | 9.980 | 1287.88 | 373.13 | 14.985 | 1226.08 |
| 343.14 | 14.981 | 1331.76 | 373.13 | 19.988 | 1273.31 |
| 343.14 | 19.987 | 1366.29 | 373.13 | 24.985 | 1310.98 |
| 343.14 | 24.987 | 1395.32 | 373.13 | 29.993 | 1342.35 |
| 343.14 | 29.984 | 1420.52 | 378.12 | 5.024 | 996.61 |
| 348.13 | 2.405 | 1142.75 | 378.13 | 9.976 | 1136.84 |
| 348.14 | 4.981 | 1200.23 | 378.12 | 14.980 | 1207.69 |
| 348.14 | 9.982 | 1268.02 | 378.12 | 19.983 | 1257.41 |
| 348.14 | 14.981 | 1314.73 | 378.12 | 24.993 | 1296.87 |
| 348.14 | 19.983 | 1351.05 | 378.12 | 29.989 | 1329.27 |
| 348.14 | 24.984 | 1381.34 | 383.12 | 5.023 | 948.71 |
| 348.14 | 29.985 | 1407.51 | 383.12 | 9.987 | 1113.06 |
| 353.13 | 2.597 | 1109.58 | 383.12 | 14.985 | 1189.19 |
| 353.13 | 4.979 | 1172.21 | 383.12 | 19.987 | 1241.58 |
| 353.13 | 9.980 | 1247.57 | 383.12 | 24.991 | 1282.61 |
| 353.13 | 14.980 | 1297.46 | 383.12 | 29.991 | 1316.25 |
| 353.14 | 19.983 | 1335.71 | 388.11 | 5.023 | 893.37 |
| 353.13 | 24.984 | 1367.34 | 388.12 | 9.978 | 1088.27 |
| 353.13 | 29.985 | 1394.49 | 388.12 | 14.980 | 1170.38 |
| 358.13 | 2.805 | 1074.04 | 388.12 | 19.982 | 1225.58 |
| 358.13 | 5.023 | 1143.42 | 388.12 | 24.983 | 1268.15 |
| 358.13 | 10.023 | 1227.12 | 388.12 | 29.992 | 1303.22 |
| 358.13 | 14.986 | 1279.96 | 393.11 | 5.020 | 828.75 |
| 358.13 | 19.980 | 1320.25 | 393.12 | 9.983 | 1063.00 |
| 358.13 | 24.990 | 1353.32 | 393.12 | 14.984 | 1151.47 |
| 358.14 | 29.984 | 1381.46 | 393.12 | 19.982 | 1209.56 |
| 363.13 | 3.028 | 1035.55 | 393.12 | 24.983 | 1253.59 |
| 363.13 | 4.978 | 1110.23 | 393.12 | 29.983 | 1290.18 |
| 363.13 | 9.988 | 1205.13 | 398.11 | 5.024 | 754.15 |
| 363.13 | 14.988 | 1262.21 | 398.12 | 9.979 | 1037.00 |
| 363.13 | 19.983 | 1304.69 | 398.12 | 14.980 | 1132.27 |
| 363.13 | 24.992 | 1339.27 | 398.12 | 19.986 | 1193.46 |
| 363.13 | 29.992 | 1368.46 | 398.12 | 24.984 | 1239.38 |
| 368.12 | 3.268 | 994.09 | 398.12 | 29.983 | 1277.19 |
| 368.13 | 4.989 | 1075.74 | 403.10 | 5.024 | 673.74 |
| 368.13 | 9.982 | 1182.97 | 403.11 | 9.983 | 1010.47 |
| 368.13 | 14.981 | 1244.15 | 403.11 | 14.979 | 1112.93 |
| 368.13 | 19.987 | 1289.06 | 403.11 | 19.981 | 1177.31 |
| 368.13 | 24.979 | 1325.08 | 403.11 | 24.992 | 1225.23 |

Table I. (Continued)

| T (K) | P (MPa) | ho (kg · m ⁻³) | <i>T</i> (K) | P (MPa) | ho (kg·m ⁻³) |
|--------|---------|----------------------------|--------------|---------|--------------------------|
| 403.11 | 29.986 | 1264.28 | 443.11 | 5.024 | 354.25 |
| 408.10 | 5.024 | 597.48 | 443.10 | 9.982 | 786.06 |
| 408.11 | 9.983 | 983.24 | 443.10 | 14.984 | 955.13 |
| 408.11 | 14.983 | 1093.49 | 443.10 | 19.981 | 1047.90 |
| 408.11 | 19.985 | 1161.17 | 443.10 | 24.982 | 1112.03 |
| 408.11 | 24.986 | 1210.98 | 443.10 | 29.992 | 1161.52 |
| 408.11 | 29.994 | 1251.46 | 448.10 | 5.017 | 338.51 |
| 413.11 | 5.023 | 534.68 | 448.10 | 9.980 | 758.88 |
| 413.11 | 10.023 | 956.84 | 448.10 | 14.982 | 935.64 |
| 413.11 | 15.021 | 1074.53 | 448.10 | 19.982 | 1031.91 |
| 413.11 | 19.982 | 1144.91 | 448.10 | 24.991 | 1098.18 |
| 413.11 | 24.983 | 1196.73 | 448.10 | 29.983 | 1148.97 |
| 413.11 | 29.984 | 1238.61 | 453.10 | 5.022 | 325.91 |
| 418.11 | 5.024 | 485.45 | 453.10 | 9.981 | 732.97 |
| 418.11 | 9.983 | 927.35 | 453.10 | 14.982 | 916.25 |
| 418.11 | 14.986 | 1054.21 | 453.10 | 19.982 | 1016.06 |
| 418.11 | 19.982 | 1128.69 | 453.10 | 24.984 | 1084.37 |
| 418.11 | 24.983 | 1182.52 | 453.10 | 29.983 | 1136.56 |
| 418.11 | 29.980 | 1224.97 | 458.10 | 5.023 | 314.26 |
| 423.11 | 5.024 | 447.27 | 458.10 | 9.983 | 707.99 |
| 423.11 | 9.979 | 898.78 | 458.10 | 14.982 | 897.08 |
| 423.11 | 14.981 | 1034.31 | 458.10 | 19.983 | 1000.33 |
| 423.11 | 19.983 | 1112.47 | 458.10 | 24.984 | 1070.68 |
| 423.11 | 24.990 | 1168.36 | 458.10 | 29.985 | 1124.23 |
| 423.11 | 29.988 | 1212.06 | 463.10 | 5.021 | 303.52 |
| 428.10 | 5.024 | 416.97 | 463.10 | 9.980 | 684.14 |
| 428.10 | 9.976 | 870.10 | 463.10 | 14.981 | 878.23 |
| 428.11 | 14.977 | 1014.40 | 463.10 | 19.986 | 984.70 |
| 428.11 | 19.980 | 1096.21 | 463.10 | 24.982 | 1057.04 |
| 428.11 | 24.984 | 1154.19 | 463.10 | 29.984 | 1111.96 |
| 428.11 | 29.991 | 1199.42 | 468.10 | 5.024 | 294.24 |
| 433.11 | 5.024 | 392.35 | 468.10 | 9.999 | 662.43 |
| 433.11 | 9.984 | 841.95 | 468.10 | 15.022 | 860.83 |
| 433.11 | 14.987 | 994.77 | 468.10 | 20.018 | 969.89 |
| 433.11 | 19.984 | 1080.09 | 468.10 | 24.980 | 1043.50 |
| 433.11 | 24.985 | 1140.07 | 468.10 | 29.986 | 1099.82 |
| 433.11 | 29.988 | 1186.74 | 473.10 | 5.024 | 285.44 |
| 438.10 | 5.024 | 371.77 | 473.10 | 9.986 | 640.32 |
| 438.10 | 9.984 | 813.80 | 473.10 | 14.983 | 841.49 |
| 438.10 | 14.981 | 974.78 | 473.10 | 19.981 | 954.02 |
| 438.10 | 19.987 | 1064.03 | 473.10 | 24.990 | 1030.23 |
| 438.10 | 24.983 | 1126.03 | 473.10 | 29.992 | 1087.84 |
| 438.10 | 29.982 | 1174.05 | | | |

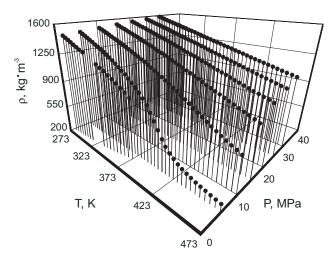


Fig. 1. Experimental densities of 1,1,1,2,3,3,3-heptafluoropropane (R227ea).

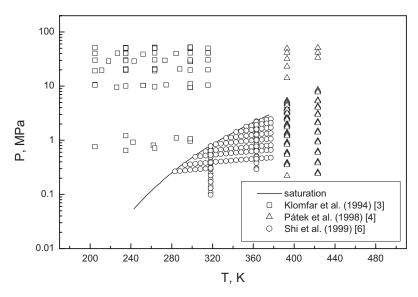


Fig. 2. *PT* diagram of the experimental density data for 1,1,1,2,3,3,3-hepta-fluoropropane (R227ea) from Klomfar et al. [3], Pátek et al. [4], and Shi et al. [6].

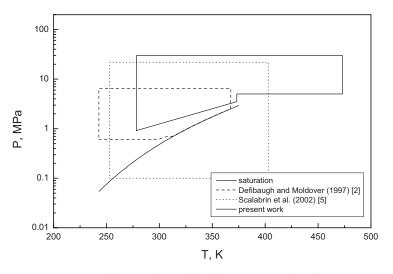


Fig. 3. *PT* range of the experimental data for 1,1,1,2,3,3,3-heptafluoropropane (R227ea) covered by the experimental data of Defibaugh and Moldover [2] and Scalabrin et al. [5].

A virial-type EoS

$$P = T\rho[R + B\rho + C\rho^{2} + D\rho^{3} + E\rho^{4} + F\rho^{5}]$$
(1)

with the following temperature dependent functions

$$B = a_1 - \frac{a_2}{T} - \frac{a_3}{T^2} - \frac{a_4}{T^3} - \frac{a_5}{T^4}$$
(2)

$$C = a_6 + \frac{a_7}{T} + \frac{a_8}{T^2} \tag{3}$$

$$D = a_9 + \frac{a_{10}}{T}$$
(4)

$$E = a_{11} + \frac{a_{12}}{T} \tag{5}$$

and

$$F = \frac{a_{13}}{T} \tag{6}$$

| | Units: K, MPa, an | d mol·L | |
|------------------|-------------------|----------------|-----------------------------|
| $T_{ m min}$ | 278.2 | a_1 | 0.0038995467 |
| $T_{\rm max}$ | 473.1 | a_2 | 2.9150189 |
| P _{min} | 0.92 | a_3 | -227.01468 |
| P _{max} | 30.02 | a_4 | 1634.4828 |
| $ ho_{ m min}$ | 1.68 | a_5 | -41.013512 |
| $\rho_{\rm max}$ | 9.34 | a_6 | $-2.7773051 \times 10^{-5}$ |
| data points | 257 | a ₇ | -0.022646112 |
| RMSD (density) | 0.0041 | a_8 | -13.960742 |
| RMSDr (density) | 0.0626 | a_9 | $-5.0776465 \times 10^{-5}$ |
| bias (density) | -0.000023 | a_{10} | 0.095528176 |
| RMSD (pressure) | 0.0887 | a_{11} | 1.3543942×10^{-5} |
| RMSDr (pressure) | 2.5859 | a_{12} | -0.019939767 |
| bias (pressure) | 0.00525 | a_{13} | 0.0010457274 |
| | | | |

Table II. Parameters for the Virial Equation for 1,1,1,2,3,3,3-Heptafluoropropane (R227ea):Temperature, Pressure and Density Range, EoS Parameters and Statistical Values,Units: K. MPa. and mol·L⁻¹

was employed for the correlation of the measured $P\rho T$ data in the sub- and supercritical states. The equation is a reduced version of the Benedict– Webb–Rubin-type Bender EoS [12]. In this equation, the exponential term of the Bender equation was omitted, so that the number of parameters was reduced from 20 to 13. The data were correlated by least squares minimization using the following objective function.

$$S = \sum_{i} \left[\left(\rho_{i, \exp} - \rho_{i, \operatorname{calc}} \right) / \rho_{i, \exp} \right]^2 \tag{7}$$

In Table II, the 13 parameters of the EoS together with additional statistical values and the validity range are given. The absolute (RMSD) and relative (RMSDr) root-mean-square deviations, and the mean deviation (bias) for the density and for the pressure were calculated. In Fig. 4, the relative deviations between the experimental and the correlated values are shown. The deviations are usually within $\pm 0.2\%$. As expected, near the critical point at about $T_c = 374.88$ K and $P_c = 2.934$ MPa [13], higher deviations are observed. It is strongly recommended to use the equation parameters only within the temperature, pressure, and density ranges covered by the correlation (compressed liquid and supercritical states) and only for the calculation of $P\rho T$ properties.

Recently, an EoS for the $P\rho T$ surface has been published for R227ea [13], valid in the range of the cited references. This equation results from the combination of the ECS method and of the neural networks technique,

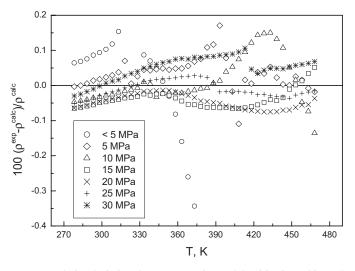


Fig. 4. Relative deviations between experimental densities from this work and the EoS correlation for 1,1,1,2,3,3,3-heptafluoropropane (R227ea).

and from now on, it will be referred to as the "ECS-NN" EoS. The cited ECS-NN EoS is a multiparameter equation of state of high accuracy dedicated to the whole thermodynamic surface of R227ea. Further more, it has a correlative nature being heuristically based solely on experimental data, and from this point of view, it is competitive with the well known Schmidt–Wagner technique for the development of a dedicated EoS in the Helmholtz energy optimized form. This EoS has been based, on purpose, on only density data, but it represents with high accuracy any thermodynamic quantity, as was demonstrated in the cited paper by Scalabrin et al. [13]. On the occasion of the publication of the new density data of the present work, that EoS has been selected as a reference one, with respect to which to check the data reliability.

For the regression of the ECS-NN EoS parameters, the density sources of Klomfar et al. [3], Pátek et al. [4], Scalabrin et al. [5], and Shi et al. [6] were used, whereas the data from Defibaugh and Moldover [2] and the data of the present work were not considered in the regression. A comprehensive validation of the cited data sources was then carried out for the present correlation, Eq. (1), and the ECS-NN EoS [13]. For the validation, only the points within the validity range of Eq. (1) were selected. The validation results are reported in Table III. In the validity range limits of these data the cited ECS-NN EoS and the present Eq. (1) reach an equivalent level of accuracy in the representation of the literature $P\rho T$ data.

| | | | | | | | EoS correlation this work | | | ECS-NN EoS | | | |
|--------------------|-----|------------|-----|-------------|------------------|------------------|---------------------------|-------------|------------|------------|-------------|------------|------|
| Phase ^a | | ange K) | | ange Pa) | NPT ^b | NPR ^c | AAD (%) | Bias (%) | Max (%) | AAD (%) | Bias (%) | Max (%) | Ref. |
| 1 | 243 | 367 | 0.6 | 6.5 | 1014 | 636 | 0.05 | 0.00 | -0.24 | 0.13 | 0.13 | 0.24 | [2] |
| 1 | 205 | 315 | 0.2 | 51 | 83 | 19 | 0.25 | -0.22 | -0.45 | 0.06 | 0.05 | 0.19 | [3] |
| 1 | 253 | 374 | 0.2 | 20 | 6888 | 4835 | 0.16 | -0.15 | 0.70 | 0.06 | 0.05 | 0.85 | [5] |
| 1 | 278 | 373 | 0.9 | 30 | 137 | 137 | 0.04 | 0.00 | -0.34 | 0.27 | 0.27 | 0.47 | d |
| sc | 374 | 403 | 0.1 | 22 | 2811 | 2279 | 4.46 | -4.05 | -47 | 4.74 | -4.74 | -46 | [5] |
| sc | 393 | 423 | 0.2 | 50 | 81 | 26 | 4.13 | 3.93 | 14.17 | 0.87 | 0.41 | 4.49 | [4] |
| sc | 383 | 473 | 5 | 30 | 120 | 120 | 0.05 | 0.00 | 0.17 | 0.36 | 0.31 | -0.73 | d |
| | 0 | verall | | | 11134 | 8052 | 1.38 | -1.22 | -47 | 1.40 | - 1.29 | - 46 | |

Table III.Validation Results of the EoS Correlation, Eq. (1), and of the ECS-NN EoS [13]Versus Experimental $P\rho T$ Data

^{*a*} l, liquid; sc, supercritical.

^b NPT: total number of points.

^c NPR: number of points falling inside the validity range of the EoS correlation.

^d This work.

The present correlation, regressed only to the data of the present work, agree within $\pm 0.2\%$ with the literature data for the liquid phase. In the supercritical region, greater deviations are found with respect to the references of Pátek et al. [4] and Scalabrin et al. [5].

In the development of the ECS-NN dedicated EoS for R227ea the data of Scalabrin et al. [5] for the supercritical region were not included in the primary data sets because of their lower experimental accuracy. They have been anyway assumed for validation of the present Eq. (1) in the same region, but with expected higher deviations. The same result is also obtained with respect to the reference ECS-NN EoS; see Table III.

The deviations between the present correlation, Eq. (1), and some experimental data sources are plotted in Figs. 5 and 6 for the liquid and supercritical states, respectively. In the liquid phase, the data of Defibaugh and Moldover [2] are represented very well, while the data of Klomfar et al. [3] show greater and biased deviations. It must be recalled that, before the validation, a screening was done in which the data points outside the temperature or pressure validity range of Eq. (1) were excluded. So the validation was performed on points with temperatures or pressures very similar to those of the present work. Thus, the deviations between Eq. (1) and the literature data sources, reported in Table III and in Figs. 5 and 6, are not caused by temperature or pressure extrapolations.

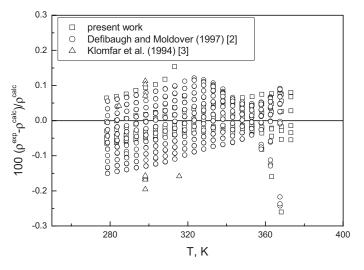


Fig. 5. Relative deviations between published experimental densities and the EoS correlation (Eq. (1)) for 1,1,1,2,3,3,3-heptafluoropropane (R227ea) (liquid phase).

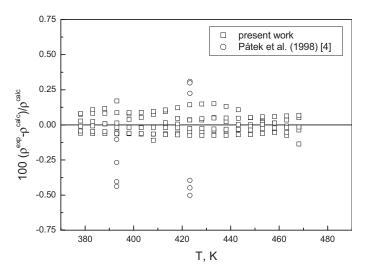


Fig. 6. Relative deviations between published experimental densities and the EoS correlation (Eq. (1)) for 1,1,1,2,3,3,3-heptafluoropropane (R227ea) (supercritical phase) (Outliers up to 4% are not shown).

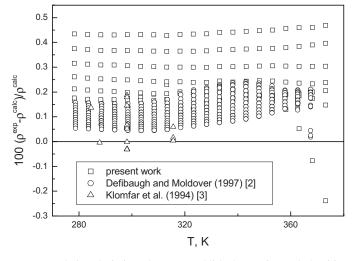


Fig. 7. Relative deviations between published experimental densities and the ECS-NN EoS for 1,1,1,2,3,3,3-heptafluoropropane (R227ea) (liquid phase).

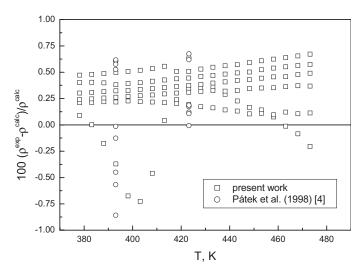


Fig. 8. Relative deviations between published densities and the ECS-NN EoS for 1,1,1,2,3,3,3-heptafluoropropane (R227ea) (supercritical phase) (Outliers up to 4.5% are not shown).

Table III shows that the ECS-NN method gives a good and balanced performance with regard to all data sets, with the exception of the data of Scalabrin et al. [5] in the supercritical phase. The average deviations of the present data set from the ECS-NN method are 0.27% in the liquid and 0.36% in the supercritical zone. The results of the ECS-NN validation are plotted in Figs. 7 and 8, respectively, for the liquid and supercritical states. In order to allow a homogeneous comparison with the correlation of the present work, the validation was conducted on the same data points selected for the validation of Eq. (1). With the exception of the present data, all of the other data sources in the supercritical region show much larger deviations than for the liquid state.

4. CONCLUSIONS

Reliable compressed liquid and supercritical densities of 1,1,1,2,3,3,3heptafluoropropane (R227ea) were measured with the help of a computeroperated vibrating tube densimeter. For the correlation of the experimental data a virial-type EoS was employed. With the parameters given in Table II the data can be described within experimental uncertainty. By comparison with the data of other authors and also with the ECS-NN EoS, the quality of the experimental procedure was validated, so that the obtained parameters can be recommended to describe the $P\rho T$ behavior of R227ea in the covered temperature and pressure range. In the future, further results for pure components and for binary mixtures will be published. The investigation of binary mixtures will demonstrate the suitability of the measurement system for the determination of mixture data, i.e., temperature and pressure dependence of the excess volumes.

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Compressed Liquid and Supercritical Densities of R227ea

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